

# Coaxial Magnetic Probes and Applications

DOUG C. SMITH, AUSPEX Systems  
RICHARD HAYNES, Richard Haynes Consultants

## INTRODUCTION

A conference was recently held by the National Institute of Standards and Technology to discuss the problems presented by the electromagnetic compliance community in the United States.<sup>1</sup> Some of the most pressing problems presented could be addressed by the appropriate applications of shielded magnetic probes.<sup>2</sup>

The principles of magnetic probe design have been applied to both circular<sup>3,4</sup> and square probes.<sup>5</sup> Simply stated, a gap in the outer shield of the coaxial cable is introduced at equal distances from the point where the inner conductor is grounded to the outer shield and the point where the loop begins.<sup>5-7</sup> By the appropriate application of transmission line theory, the resonant frequency can be calculated and does not limit the upper frequency range of interest for most electronic products and loops smaller than 2 cm in diameter.<sup>2</sup> To minimize the errors in measurement, the diameter of the loop should be less than 0.01 times the wavelength.<sup>4</sup> For material reasons this may limit loops made from coaxial cable to tens of GHz. The smaller the diameter of the loop, the better resolution of the properties of the system of interest, but sensitivity may become an issue, especially at low frequencies. The sensitivity can be enhanced by matching the probe source impedance to the measuring instrument.<sup>8</sup>

Using shielded magnetic loops to illuminate a shield for testing represents a more realistic test than using plane waves for many configura-

*Although the principles of designing shielded magnetic probes have been well established for some time, new applications continue to be developed.*

tions. Shields that are close to printed wiring boards are illuminated, for the most part, by magnetic fields that are perpendicular to the shield, and generated by the magnetic loops formed by paths on the circuit board. Testing such a shield with plane waves can lead to significant errors in the measurement of shielding effectiveness as it applies to the circuit being shielded.

## APPLICATION OF SHIELDED MAGNETIC PROBES

Although the principles of shielded magnetic probe design are well known, application of the probe design is still a fruitful area for development. A review of recent patents shows quite a number of patents that are based on new applications. Both circular and rectangular shielded magnetic probes have been applied to the following:

- measurement of homogeneity in material properties<sup>9</sup> and shielding effectiveness of materials<sup>10</sup>

- measurement of shielding effectiveness and emissions from shielding enclosures<sup>11</sup> and electronic devices<sup>12</sup>
- measurement of shielding effectiveness of interconnections used in shielded enclosures<sup>11</sup>
- verification of circuit designs for undesirable emissions and immunity of circuits to impinging electromagnetic energy<sup>6, 13, 14</sup>

When measuring the first three items, two probes are placed at a fixed distance and the material or enclosure is inserted between the probes. The insertion loss is recorded. Measurements made in this manner are independent of the circuit and are for diagnostic purposes only.<sup>2</sup> The insertion loss is referenced to the coupling strength of the probes for the same conditions without the inserted item. The figure of merit is the shielding effectiveness. Such measurements have been made for a number of materials such as electroless Ni/Cu, vapor deposited Al (with and without a protective film), arc sprayed metals/alloys, conductive paints, meshed wires, formed metals and fiber-filled plastics.<sup>10</sup> Under the appropriate conditions, the resistance/square can be calculated.<sup>9</sup>

By using the contactless shielded magnetic probes, a more exact value of shielding effectiveness and derived values of resistance can be obtained. For materials that are sensitive to the contact pressures of the probes, as in the direct measurement

of resistance, the measurement is usually not reproducible using the contact methods. Materials that are sensitive to contact probe pressures include filmed material such as oxidized Al, Ni and alloys and meshed wire composites. Materials such as fiber-filled plastics can yield very high resistance when using contact probes, but offer sufficient shielding effectiveness. In this case a high resistance surface film of plastic is present due to the material and processing conditions.

Measurements of the insertion loss of enclosures require high resolution to find the primary cause of the electromagnetic leakage, so smaller magnetic probes are used to advantage. A large frequency range is measured, even beyond the operating frequency, so small holes or other defects can be detected. Such information can then be given to the vendor so potential problems in processing and/or materials can be corrected early in the design cycle.

Verification of circuit designs is an art dependent on the availability of a good set of rectangular probes and an understanding of the various devices that can be potential radiators and receivers.<sup>12,13</sup> The area of testing of individual components and relating the relevance of such measurements to meet regulatory requirements should be expanded.<sup>12</sup>

## CIRCULAR VERSUS RECTANGULAR SHIELDED MAGNETIC PROBES

For uniform fields, only the loop area (single turn loops) affects coupling strength. A circular and a rectangular loop of the same area should have the same open circuit output voltage. Rectangular loops will have more inductance, which will have some effect on the output voltage. For analysis of most circuits, rectangular

loops have a better geometric fit than do circular probes, but at very large distances both are effectively the same. The better fit of rectangular probes to most circuits translates to better coupling between the circuit and the probe.

The lower size limit of fabrication of circular and rectangular probes using coaxial cable is better for circular probes than for rectangular ones due to the material properties of the cable.

Circular probes are bent to a small radius of curvature whereas rectangular probes have 90-degree bends, thus requiring a smaller radius of curvature than a circular probe of the same area. This limitation becomes important at very small probe sizes which approach tens of GHz frequency response.

## SUMMARY

Circular probes are useful for many purposes but rectangular probes are most useful as all-purpose probes. Rectangular probes range in usefulness from measurement of shielding effectiveness of materials, enclosures and interconnection methods to detecting the source of noise and susceptibility of a working circuit.

## REFERENCES

1. EMI/EMC Metrology Challenges for Industry, sponsored by U.S. Dept. of Commerce, National Institute of Standards and Technology, Boulder, CO, January 25-26, 1995.
2. R. Haynes and D.C. Smith, "Solutions to Problems Presented at this Workshop," EMI/EMC Metrology Challenges for Industry, sponsored by U.S. Dept. of Commerce, National Institute of Standards and Technology, Boulder, CO, January 25-26, 1995.
3. L. L. Libby, Proceedings of the IRE, September 1946, pp. 641-646.
4. I. I. Whiteside and R. W. King, IEEE Transactions on Antennas and Propagation, May, 1964, pp. 291-297.
5. D. C. Smith, "Noise Measurement Probe,"

U.S. Patent 4,879,507, November 7, 1989.

6. D. C. Smith, *High Frequency Measurements and Noise in Electronic Circuits*, (New York: Van Nostrand Reinhold, 1993) pp. 125-159.
7. H. W. Ott, *Noise Reduction Techniques in Electronic Systems*, (New York: John Wiley and Sons, 1988) pp. 60.
8. S. Roleson, EDN, May 17, 1984, p. 203.
9. J. A. Catrysse, M. de Goeije, W. Steenbakkens and L. Anat, IEEE Transactions on EMC, November 1993, p. 440.
10. D. C. Smith, C. Herring, Jr. and R. Haynes, 1994 IEEE International Symposium on Electromagnetic Compatibility, Chicago, August 22-26, 1994.
11. J. A. Catrysse, Publication of the IEE Symposium on Screening and Shielding, January 1992, pg. 4/1.
12. R. R. Goulette, R. J. Crawhall and S. K. Xavier, IEICE, pg. 124, Vol. E75-B, No. 3, March 1992.
13. D. C. Smith, High Frequency Measurements Course, 1996.
14. M. Mardiguian, *Controlling Radiated Emissions by Design*, (New York: Van Nostrand Reinhold, 1992), pp. 267-277.

**DOUGLAS C. SMITH** received a BSEE from Vanderbilt in 1969 and an MSEE from California Institute of Technology in 1970, after which he joined AT&T Bell Labs. Doug recently retired as a Distinguished Member of the technical staff. Doug is well known throughout the EMC industry as an expert in several technical areas that include EMC, ESD, EFT and other forms of pulsed electromagnetic interference, FCC Parts 15 and 68 testing and design, telephone voice frequency transmission, IC design, and computer simulation. A senior member of IEEE, Doug teaches private seminars on topics including high-frequency noise measurement techniques, system-level ESD, and pulsed electromagnetic interference. Currently Doug heads an EMC group at Auspex Systems in Santa Clara, CA and can be reached at (800) 323-3956.

**RICHARD HAYNES** graduated with a Ph.D. in electrochemistry from the University of Pennsylvania and completed a Post-Doctoral program in the areas of magnetic and electron spin resonance in metal solutions at the Laboratory for Research on the Structure of Matter. He recently retired from AT&T Bell Labs after 26 years. During this period, Richard developed expertise in metal finishing, industrial ecology, reliability, corrosion and film growth, battery technology for portable products, EMI shielding technologies and design and applications of magnetic probes to EMC. Richard is now head of Richard Haynes Consultants and can be contacted at (800) 890-4634.